

Def!  $S \subset \mathbb{R}^d$   $f: \mathbb{R}^d \rightarrow \mathbb{R}$

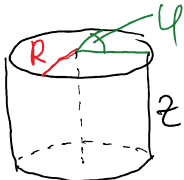
$\int_S f dV =$  mass/weight of  $S$  with density given by  $f$

In particular, if  $f \equiv 1 \Rightarrow$  volume of  $S$   
 if  $S$  has special shape  $\Rightarrow$  change of coordinates

Cylindrical coordinates,

Spherical coordinates,

$(r, \varphi, z)$  parameters  
 $\varphi \in [0, 2\pi)$   
 $r \in [0, R]$



$(r, \varphi, \vartheta)$   
 $\varphi \in [0, 2\pi)$   
 $\vartheta \in (0, \pi)$   
 $r \in [0, R]$



$x = r \cos \varphi$   
 $y = r \sin \varphi$   
 $z = z$

polar-coord. substitutions  
 $x^2 + y^2 = r^2$

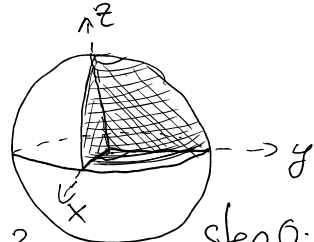
$x = r \cos \varphi \sin \vartheta$   
 $y = r \sin \varphi \sin \vartheta$   
 $z = r \cos \vartheta$

$x^2 + y^2 + z^2 = r^2$

$\boxed{r} dr d\varphi dz$   $\xrightarrow{\text{Jacobian-det.}}$   $\boxed{r^2 \sin \vartheta} dr d\varphi d\vartheta$

Ex 1  $S = \{(x, y, z) : \underbrace{x^2 + y^2 + z^2 \leq 1}_{\text{unit sphere}}, x, y, z > 0\}$

$f(x, y, z) = \sqrt{x^2 + y^2 + z^2}$   $\iiint_S f(x, y, z) dx dy dz = ?$



step 0: draw

step 1: determine which coordinates to use, determine range of parameters

here: spherical  $0 \leq r \leq 1$   $0 \leq \varphi \leq \pi/2$   $0 \leq \vartheta \leq \pi/2$

step 2: write  $f(x, y, z)$  in new coordinates

here:  $f(x, y, z) = \sqrt{r^2} = r$

step 3: integrate with substitution

$\iiint_S f(x, y, z) dx dy dz = \int_0^1 \int_0^{\pi/2} \int_0^{\pi/2} r \cdot r^2 \sin \vartheta d\vartheta d\varphi dr$

$$\begin{aligned}
 \iiint_S f(x,y,z) dx dy dz &= \int_0^1 \int_0^{\pi/2} \int_0^{\pi/2} r \cdot r^2 \sin \theta d\theta d\varphi dr \\
 &= \underbrace{\left( \int_0^1 r^3 dr \right)}_{1/4} \cdot \underbrace{\left( \int_0^{\pi/2} 1 \cdot d\varphi \right)}_{\pi/2} \cdot \underbrace{\left( \int_0^{\pi/2} \sin \theta d\theta \right)}_{[-\cos \theta]_0^{\pi/2}} = \underline{\underline{\pi/8}}
 \end{aligned}$$

Ex 2

$T := \{(x,y,z) : x^2 + y^2 \leq 1, 0 \leq z \leq x^2 + y^2\}$ 

 $\Rightarrow$  cylindrical coords

$f(x,y,z) := x^2 + y^2 = r^2$  in cylindrical  $z$  depends on  $x,y$   
 $\Rightarrow$  inner most in integration

$$\iiint_T f dx dy dz = \int_0^1 \int_0^{2\pi} \int_0^{r^2} r^2 \cdot r dz d\varphi dr$$

$$= \left( \int_0^{2\pi} 1 d\varphi \right) \cdot \int_0^1 r^3 \left( \int_0^{r^2} 1 dz \right) dr = 2\pi \cdot \int_0^1 r^5 dr = \underline{\underline{\pi/3}}$$

Reference: Thomas' Calculus Ch. 16.2

Def<sup>n</sup> **vector field**  $\vec{F} = \vec{F}(x, y, z) = (F_1(x, y, z), F_2(x, y, z), F_3(x, y, z))$   
 is an  $\mathbb{R}^3 \rightarrow \mathbb{R}^3$  mapping, i.e. a vector  $(F_1, F_2, F_3)$  is assigned to each point of 3d space

Notation position vector  $\underline{r} = (x, y, z)$   $r = |\underline{r}| = \sqrt{x^2 + y^2 + z^2}$

Ex<sup>1</sup>  $\hookrightarrow f(x, y, z) = x^2 y \sin z$  is NOT a vector field, since  $f$  assigns a number/scalar to each point of space  $\rightarrow$  scalar field  
 But  $\text{grad } f = \left( \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right) = (2xy \sin z, x^2 \sin z, x^2 y \cos z)$   
 is a vector field  $\rightarrow$  **gradient field** (important later)

$\hookrightarrow$  physical interpretations:

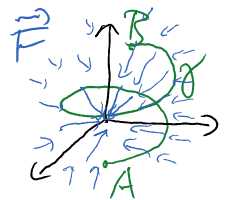
**force field**:  $\vec{F}(\underline{r})$  gives the force in each point  $\underline{r}$

eg. electromagnetic field or gravitational force, for some  $k > 0$

$$\vec{F}(\underline{r}) = -k \frac{\underline{r}}{r^3} \quad \text{or} \quad \vec{F}(x, y, z) = \left( \frac{-kx}{(x^2 + y^2 + z^2)^{3/2}}, \frac{-ky}{(x^2 + y^2 + z^2)^{3/2}}, \frac{-kz}{(x^2 + y^2 + z^2)^{3/2}} \right)$$

Question given a curve  $\gamma$  in vector field  $\vec{F}$ ,

how much work is needed to get from one endpoint  $A$  of  $\gamma$  to the other  $B$ ?



**line integral**

**velocity field**:  $\vec{F}(\underline{r})$  gives the velocity at each point  $\underline{r}$   
 eg. flow of air in a wind tunnel or water in a pipeline

spin/rotation around  $z$ -axis (parallel to  $xy$ -axis)  
 at constant speed  $\omega$  (angular velocity)  
 $\vec{F}(x, y, z) = (-\omega y, \omega x, 0)$  velocity



$$F(x, y, z) = (-wy, wx, 0) \text{ velocity}$$



Question How much fluid leaves/enters the surface of  $S$  if the fluid is flowing according to the velocity field  $\vec{F}$ ?



surface integral



## 2. Line Integrals of Vector Fields

Tuesday, October 31, 2017 1:14 PM

Reference: Thomas' Calculus ch. 16.2-3

Def<sup>n</sup> line integral

$\gamma$  is a directed, parameterized curve in space given by

$$\mathbf{r}(t) = (x(t), y(t), z(t)) \quad a \leq t \leq b \quad A = \mathbf{r}(a) \text{ starting point}$$

$B = \mathbf{r}(b)$  endpoint

$\vec{F} = (F_1(x, y, z), F_2(x, y, z), F_3(x, y, z))$  is a vector field (interpreted as force field)

always assume  $\gamma$  is smooth, depends "nicely" on  $t$ , similarly all components of  $\vec{F}$  and partial derivatives depend "nicely" on  $x, y, z$

$$\int_{\gamma} \vec{F}(\underline{r}) d\underline{r} \stackrel{\text{other notation}}{=} \int_{\gamma} F_1 dx + F_2 dy + F_3 dz = \text{work done in moving an object from } A \text{ to } B \text{ along } \gamma \text{ against } \vec{F}$$

Thm<sup>1</sup> evaluating a line integral according to parametrization  $\mathbf{r}(t)$

$$\int_{\gamma} \vec{F}(\underline{r}) d\underline{r} = \int_a^b \vec{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$

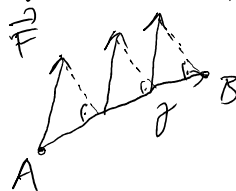
localize  $\vec{F}$  to  $\gamma$

tangent/velocity vector =  $\left( \frac{dx(t)}{dt}, \frac{dy(t)}{dt}, \frac{dz(t)}{dt} \right)$   
scalar product of the two vectors

explanation

↳ first assume  $\gamma$  is a line segment between  $A$  and  $B$  &  $\vec{F} = (F_1, F_2, F_3)$  is constant, i.e. independent of  $x, y, z$

amount of force in the direction of the movement = orthogonal projection of  $\vec{F}$  onto  $\vec{AB}$



$$= \vec{F} \cdot \frac{\vec{AB}}{|\vec{AB}|} \quad (\text{recall from lin. algebra})$$

$\vec{F}$  is constant  $\Rightarrow$  this is true for every point on  $\gamma$

$$\text{total movement is } |\vec{AB}| \Rightarrow \text{work} = \vec{F} \cdot \frac{\vec{AB}}{|\vec{AB}|} |\vec{AB}| = \vec{F} \cdot \vec{AB}$$

velocity

↳ for general curve  $\gamma$  and vector field  $\vec{F}$ :

idea is to cut up  $\gamma$  into small pieces which are "almost" line segments and  $\vec{F}$  changes only "little"; apply previous point

continue refining this subdivision to get from  $\Sigma'$  to integration a bit more formally:

- subdivide the parameter interval  $[a, b]$  into  $n$  pieces

$$a =: t_0 < t_1 < \dots < t_{n-1} < t_n =: b \quad \text{let } P_i := \mathbf{r}(t_i)$$

- replace  $(\mathbf{r}(t_i), \mathbf{r}(t_{i+1}))$  on  $\gamma$  with the line segment  $\overrightarrow{P_i P_{i+1}}$

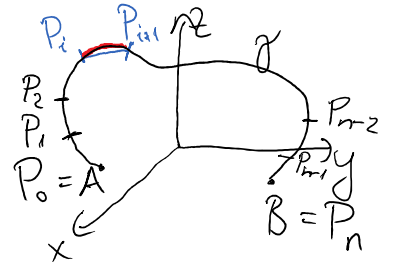
- the work on this small segment is approx

$$\approx \vec{F}(\mathbf{r}(t_i)) \cdot \overrightarrow{P_i P_{i+1}}$$

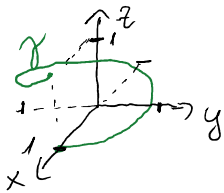
according to the previous point if we take  $\vec{F}$  constant on  $\overrightarrow{P_i P_{i+1}}$  but  $\overrightarrow{P_i P_{i+1}} = \mathbf{r}(t_{i+1}) - \mathbf{r}(t_i) \approx \mathbf{r}'(t_i) \cdot (t_{i+1} - t_i)$

- Thus the work on the whole curve is approx.

$$\approx \sum_{i=0}^{n-1} \vec{F}(\mathbf{r}(t_i)) \cdot \mathbf{r}'(t_i) \cdot (t_{i+1} - t_i) \xrightarrow[\text{refining the subdivision}]{n \rightarrow \infty} \int_a^b \vec{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$



Ex:  $\vec{F}(x, y, z) = (-y, z, 2x)$   
 $\mathbf{r}(t) = (\cos t, \sin t, t) \quad t \in [0, 2\pi]$   $\Rightarrow \vec{F}(\mathbf{r}(t)) = (-\sin t, t, 2\cos t)$   
 $\mathbf{r}'(t) = (-\sin t, \cos t, 1)$

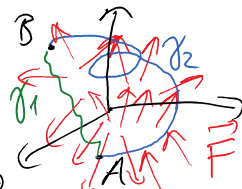


$$\int_{\gamma} \vec{F}(\mathbf{r}) d\mathbf{r} = \int_0^{2\pi} -y dx + z dy + 2x dz$$

$$= \int_0^{2\pi} \left( \underbrace{\sin^2 t}_{\frac{1-\cos 2t}{2}} + \underbrace{t \cos t + 2 \cos t}_{\text{int. by parts}} \right) dt = \left[ \frac{t}{2} - \frac{\sin 2t}{4} + t \sin t + \cos t + 2 \sin t \right]_0^{2\pi} = \pi$$

## Path independence

Question Given two different curves  $\gamma_1$  and  $\gamma_2$  between the same endpoints A and B, for what  $\vec{F}$  will the work be the same along the two different curves?



Def. The line integral is independent of the path in  $\vec{F}$  if for any two curves  $\gamma_1$  and  $\gamma_2$  (within the domain of  $\vec{F}$ ) with the same endpoints

starting point A and endpoint B  $\int_{\gamma_1} \vec{F}(\underline{r}) d\underline{r} = \int_{\gamma_2} \vec{F}(\underline{r}) d\underline{r}$ . (1)

In this case we call  $\vec{F}$  a **conservative field**.

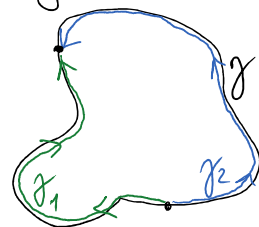
• Assume  $\vec{F}$  is a gradient field, i.e.  $\vec{F} = \text{grad} f$  for some  $f: \mathbb{R}^3 \rightarrow \mathbb{R}$ .  
We call  $f$  the **potential function** for  $\vec{F}$ .

Remark 1. Condition (1) holds if and only if for any closed loop  $\gamma$

$\oint_{\gamma} \vec{F}(\underline{r}) d\underline{r} = 0$ . Indeed, any closed  $\gamma$

can be written as the union of  $\gamma_1$  and  $\gamma_2$

so that  $\oint_{\gamma} \vec{F} d\underline{r} = \int_{\gamma_1} \vec{F} d\underline{r} - \int_{\gamma_2} \vec{F} d\underline{r}$



• In a conservative field  $\int_{\gamma} \vec{F} d\underline{r}$  only depends on the endpoints of  $\gamma$ .

Thm 2. Assume  $\vec{F}$  is a vector field on some domain of space with continuous components. Then

$\vec{F}$  is conservative  $\iff \vec{F}$  is a gradient field for some differentiable potential  $f$ .

In this case, for any smooth curve  $\gamma$  in the domain of  $\vec{F}$  parameterized by  $\underline{r}(t)$ ,  $a \leq t \leq b$ , joining points  $A = \underline{r}(a)$  with  $B = \underline{r}(b)$

$$\int_{\gamma} \vec{F}(\underline{r}) d\underline{r} = f(B) - f(A) \quad (2)$$

Remark 2 If  $\vec{F}$  is a gradient field, then (2) shows that the line integral only depends on the value of the potential function at the endpoints. Thus independent of the path itself  $\implies$  conservative.

Other direction (conservative  $\implies$  gradient field) slightly more involved.

proof (of (2)) Simple application of the Newton-Leibnitz formula

$\vec{F} = \text{grad} f$  for some potential,  $\gamma$  parameterized by  $\underline{r}(t)$   $a \leq t \leq b$

Define  $g: [a, b] \rightarrow \mathbb{R}$   $g(t) = f(\underline{r}(t))$ . By the chain rule

$$\frac{d}{dt} g(t) = (\text{grad} f)(\underline{r}(t)) \cdot \dot{\underline{r}}(t) = \vec{F}(\underline{r}(t)) \cdot \dot{\underline{r}}(t).$$

Let  $\gamma(t) = (x(t), y(t), z(t))$  be a smooth curve in  $\mathbb{R}^3$  with initial point  $A$  and terminal point  $B$ .

$$\frac{d}{dt} g(t) = (\text{grad } f)(\gamma(t)) \cdot \dot{\gamma}(t) = \underbrace{\vec{F}(\gamma(t)) \cdot \dot{\gamma}(t)}_{g'(t)}$$

Then by the Newton-Leibnitz formula

$$f(B) - f(A) \stackrel{\text{def. of } g}{=} g(b) - g(a) = \int_a^b g'(t) dt = \int_a^b \vec{F}(\gamma(t)) \cdot \dot{\gamma}(t) dt \stackrel{\text{Thm 8}}{=} \int_{\gamma} \vec{F} \cdot d\vec{r} \quad \square$$

Question How to determine whether  $\vec{F}$  is conservative and if it is, then how to determine the potential function of  $\vec{F}$ ?

### 3. Curl-test and finding a potential

Wednesday, November 1, 2017 11:20 AM

Def! *curl/rotation* of a vector field  $\vec{F}$  notation  $\text{curl}(\vec{F})$ ,  $\text{rot}(\vec{F})$

If  $\vec{F}: \mathbb{R}^2 \rightarrow \mathbb{R}^2$  is defined in the plane

$$\vec{F}(x,y) = (F_1(x,y), F_2(x,y)) \text{ then } \boxed{\text{curl}(\vec{F}) = \frac{\partial}{\partial x} F_2 - \frac{\partial}{\partial y} F_1} \text{ (is a real number)}$$

$$\nabla \vec{F} = \text{grad } \vec{F}$$

If  $\vec{F}(x,y,z) = (F_1, F_2, F_3)$  is defined in  $\mathbb{R}^3$ , then  $\text{rot}(\vec{F})$  is the vector

$$\boxed{\text{rot}(\vec{F}) = \left( \frac{\partial}{\partial y} F_3 - \frac{\partial}{\partial z} F_2, \frac{\partial}{\partial z} F_1 - \frac{\partial}{\partial x} F_3, \frac{\partial}{\partial x} F_2 - \frac{\partial}{\partial y} F_1 \right)}$$

$$= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ F_1 & F_2 & F_3 \end{vmatrix} \text{ "symbolic determinant" } = \nabla \times \vec{F}$$

$\partial_x$  is shorthand for  $\frac{\partial}{\partial x}$

Remark!  $\text{curl } \vec{F}$  has to do with how the fluid circulates close to the point  $(x,y,z)$

Observe  $\text{rot}$  in the plane is the same as the third component of  $\text{rot}$  in space.

If it is zero (number or vector), then there is no rotation.

In the plane if  $\text{rot}(\vec{F}) > 0 \rightarrow$  rotation counter clockwise

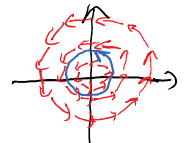
$< 0 \rightarrow$  rotation clockwise

also called *circulation density*

Ex! In the plane

$$\vec{F}(x,y) = (-\omega y, \omega x) \text{ rotation, } \omega > 0 \quad \text{curl}(\vec{F}) = \omega - (-\omega) = 2\omega > 0$$

$$\vec{F}(x,y) = (-y, 0) \text{ shear, } \text{curl}(\vec{F}) = -1 < 0$$



• In space

$$\vec{F} = \text{gravitational field} = -k \cdot \frac{\vec{r}}{r^3}$$

$$\text{curl } \vec{F} = 3(x^2+y^2+z^2)^{5/2} \cdot \hat{k} (yz - yz, -xz + xz, xy - xy) = (0, 0, 0) \text{ no rotation}$$

in general let  $f: \mathbb{R}^3 \rightarrow \mathbb{R}$  be twice continuously differentiable,  $\vec{F} = \text{grad } f$

$$\text{then } \text{curl } \vec{F} = \nabla \times \nabla f = (f''_{zy} - f''_{yz}, f''_{xz} - f''_{zx}, f''_{yx} - f''_{xy}) = (0, 0, 0)$$

$\Rightarrow$  If  $\vec{F}$  is conservative, then  $\text{rot } \vec{F}$  must be  $(0, 0, 0)$ .

Curl test In the plane and space gives sufficient (but not necessary) conditions for a vector field to be conservative.

1) We just saw: If  $\text{rot}(\vec{F}) \neq 0$  or  $(0,0,0)$  in at least one point the  $\vec{F}$  is **NOT** conservative.

(ex. rotation and shear are not conservative as we expect)

2)  $\text{rot} \vec{F} \equiv 0$  or  $(0,0,0)$  and

(a) in the plane:  $\vec{F}$  and the partial derivatives  $\partial_x F_1, \partial_y F_1, \partial_x F_2, \partial_y F_2$  are defined at every point of the plane  $\Rightarrow \vec{F}$  **IS** conservative

If this fails (at least one of the partial derivatives isn't defined in at least one point)  $\Rightarrow$  test is **INCONCLUSIVE**

(b) in space:  $\vec{F}$  and all nine partial derivatives are defined in all, but except perhaps a finite number of points of space  $\Rightarrow \vec{F}$  **IS** conservative  
 $\uparrow$  ex. just the origin

If this fails (ex. a line or plane going through the origin)  $\Rightarrow$  test is **INCONCLUSIVE**

Ex.  $\vec{F} = \left( \frac{-y}{x^2+y^2}, \frac{x}{x^2+y^2}, 2 \right)$  is it conservative?

First calculate  $\text{rot} \vec{F}$ :

$$\text{rot}(\vec{F}) = \left( \underbrace{\partial_y F_3 - \partial_z F_2}_{=0}, \underbrace{\partial_z F_1 - \partial_x F_3}_{=0}, \underbrace{\frac{x^2+y^2 - 2x^2 - (-(x^2+y^2) - (y)2y)}{(x^2+y^2)^2}}_{=0} \right) = (0,0,0) \quad \checkmark$$

But  $\vec{F}$  is not defined where  $x^2+y^2=0$ , i.e. on the z-axis  
 $\Rightarrow$  curl test is inconclusive

First two coordinates  $(-y, x)$  resemble the spin/rotation field  $\rightarrow$  guess: not cons.

From Remark 2.1. we know that  $\vec{F}$  not cons.  $\Leftrightarrow \exists$  closed  $\gamma: \oint_{\gamma} \vec{F} \cdot d\vec{r} \neq 0$

take the curve  $\gamma$  parameterized by  $\underline{r}(t) = (\cos t, \sin t, 0)$   $0 \leq t \leq 2\pi$

Then  $\vec{F}(\underline{r}(t)) = \left( \frac{-\sin t}{1}, \frac{\cos t}{1}, 2 \right)$ ,  $\dot{\underline{r}}(t) = (-\sin t, \cos t, 0)$

$$\text{Thus } \oint_C \vec{F} \cdot d\vec{r} = \int_0^{2\pi} (\underbrace{\sin^2 t + \cos^2 t}_=1) dt = 2\pi \neq 0 \Rightarrow \vec{F} \text{ is } \underline{\text{NOT}} \text{ conservative}$$

Finding a potential function  $\vec{F} = (F_1, F_2, F_3)$  is given

$$\vec{F} = (f'_x, f'_y, f'_z) \quad f = ? \quad \left\{ \begin{array}{l} \int F_1(x, y, z) dx + g_1(y, z) \\ \int F_2(x, y, z) dy + g_2(x, z) \\ \int F_3(x, y, z) dz + g_3(x, y) \end{array} \right\} \begin{array}{l} \text{combining these we} \\ \text{can determine } g_1, g_2, g_3 \\ \text{thus obtain } f(x, y, z) \end{array}$$

Ex 3.  $\vec{F}(x, y, z) = (1+4y+5z, 2+4x, 3+5x)$  is it cons? If yes, give a potential!

$$\text{rot}(\vec{F}) = (0-0, 5-5, 4-4) \equiv (0, 0, 0), \text{ everything is well-defined} \Rightarrow \underline{\text{YES}} \text{ cons.}$$

$$\text{potential: } \left. \begin{array}{l} \int F_1 dx = x + 4xy + 5xz + g_1(y, z) \\ \int F_2 dy = 2y + 4xy + g_2(x, z) \\ \int F_3 dz = 3z + 5xz + g_3(x, y) \end{array} \right\} \begin{array}{l} g_1(y, z) = 2y + 3z \\ g_2(x, z) = 5xz + x + 3z \\ g_3(x, y) = 4xy + x + 2y \end{array}$$

$$\Rightarrow \underline{f(x, y, z) = x + 2y + 3z + 4xy + 5xz + \text{const.}}$$

## 4. Surface integrals

Wednesday, November 8, 2017 3:00 PM

# Surface Integrals

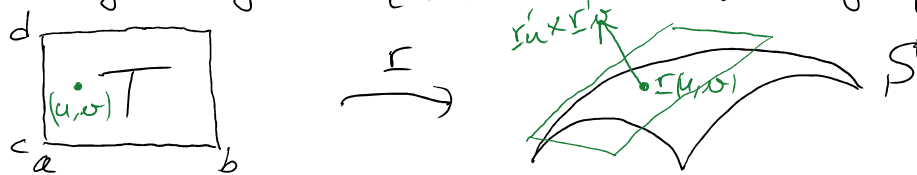
Reference Thomas' Calculus Ch 16.5-6

### Surface given by parametrization

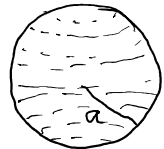
parameters  $a \leq u \leq b$   
 $c \leq v \leq d$   $T = [a, b] \times [c, d] =$  parameter domain

parametrization  $\mathbf{r}: T \rightarrow \mathbb{R}^3$   $\mathbf{r}(u, v) = (x(u, v), y(u, v), z(u, v))$

surface  $S$  given by  $\mathbf{r}$  is  $\{\mathbf{r}(u, v) : (u, v) \in T\} =$  range of  $\mathbf{r}$



tangent plane at point  $\mathbf{r}(u, v)$  is spanned by  $\begin{cases} \mathbf{r}'_u = (\partial_u x, \partial_u y, \partial_u z) \\ \mathbf{r}'_v = (\partial_v x, \partial_v y, \partial_v z) \end{cases}$   
 normal vector at  $\mathbf{r}(u, v)$  is  $\mathbf{r}'_u \times \mathbf{r}'_v$

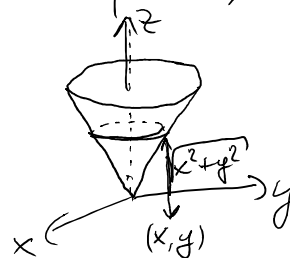
Ex sphere  $x^2 + y^2 + z^2 = a^2$   with the spherical coords.  
 $r = a$  is fixed  
 $0 \leq \varphi \leq 2\pi$   $0 \leq \vartheta \leq \pi$

Thus  $\mathbf{r}(\varphi, \vartheta) = (a \cos \varphi \sin \vartheta, a \sin \varphi \sin \vartheta, a \cos \vartheta)$

cone  $z = \sqrt{x^2 + y^2}$   $0 \leq z \leq 1$

cylindrical coords.

$0 \leq r \leq 1$   $0 \leq \varphi \leq 2\pi$   
 $z = r$



thus  $\mathbf{r}(r, \varphi) = (r \cos \varphi, r \sin \varphi, r)$

Def surface integral Assume a surface  $S \subset \mathbb{R}^3$  is given by the



parametrization  $\mathbf{r}(u,v)$  on some domain  $T \subset \mathbb{R}^2$ .  $S$  can be oriented by either taking  $\mathbf{n}(u,v) = \mathbf{r}'_u \times \mathbf{r}'_v$  or  $\mathbf{n}(u,v) = -\mathbf{r}'_u \times \mathbf{r}'_v$  at every point.  $\vec{F}$  is a "nice" vector field (at least twice differentiable).

Then the surface integral  $\equiv$  flux

$\iint_S \vec{F} d\vec{A}$  = the volume of fluid which flows through  $S$  in unit time according to the velocity field  $\vec{F}$  in the direction of the orientation.

flux  $\begin{cases} > 0 \Rightarrow \text{more fluid flows in the direction of orientation.} \\ < 0 \Rightarrow \text{more in the opposite direction} \\ = 0 \Rightarrow \text{it is even both directions} \end{cases}$

Then Depending on the orientation of  $S$

$$\iint_S \vec{F} d\vec{A} = \iint_T \underbrace{\vec{F}(\mathbf{r}(u,v)) \cdot \mathbf{n}(u,v)}_{(*)} du dv \quad (1)$$

In particular, if  $(*)$  is the same constant  $q$  for every  $(u,v) \in T$  (that is, the length of the orthogonal projection of  $\vec{F}$  onto the normal vector (w.r.t. the orientation)  $\mathbf{n}$  is the same)

then  $\iint_S \vec{F} d\vec{A} = q \cdot \iint_T 1 \cdot du dv = q \cdot \text{surface}(S) \quad (2)$

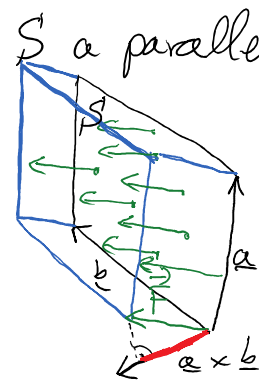
explanation very similar to the line integral

First consider  $\vec{F}$  constant everywhere and  $S$  a parallelogram spanned by the vectors  $\underline{a}$  and  $\underline{b}$ .

Flux = volume of blue parallelepipedon

= area( $S$ )  $\cdot$  height =  $|\underline{a} \times \underline{b}| \cdot \vec{F} \cdot \frac{\underline{a} \times \underline{b}}{|\underline{a} \times \underline{b}|}$

$\Rightarrow \iint_S \vec{F} d\vec{A} = \vec{F} \cdot (\underline{a} \times \underline{b})$



$$\Rightarrow \iint_S \vec{F} d\vec{A} = \vec{F} \cdot (\underline{a} \times \underline{b})$$



In general the usual method. Split the surface  $S$  into many very small pieces. Instead of the piece, consider the corresponding parallelogram in the tangent space. On this small parallelogram we consider  $\vec{F}$  constant. Hence we are in the previous setting.

Summing up over all small pieces and refining the subdivision we get

$$\iint_S \vec{F} d\vec{A} = \lim_{\substack{\Delta u \rightarrow 0 \\ \Delta v \rightarrow 0}} \sum \vec{F}(r(u,v)) \cdot (r'_u \times r'_v) \Delta u \Delta v = \iint_T \vec{F}(r(u,v)) \cdot (r'_u \times r'_v) du dv$$

If the orientation points towards  $-(r'_u \times r'_v)$ , the flux =  $(-1) \cdot$  this

'[]'

Ex 1 (to use (1)) Let  $S$  be the surface given by the parametrization

$$r(u,v) = (u+2v, -v, u^2+3v) \text{ with domain } T: 0 \leq u \leq 3 \text{ \& } 0 \leq v \leq 1.$$

$S$  is oriented so that  $\underline{n}$  points "upwards" (ie. its third component is positive)

$$\vec{F}(x,y,z) = (xy, 2x+y, z). \text{ Determine } \iint_S \vec{F} d\vec{A}!$$

↳ step 1: localize  $\vec{F}$  to the surface, ie.  $x = u+2v, y = -v, z = u^2+3v$

$$\vec{F}(r(u,v)) = ((u+2v)(-v), 2(u+2v)-v, u^2+3v)$$

↳ step 2: determine the normal vector according to the orientation given

$$r'_u \times r'_v = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ 1 & 0 & 2u \\ 2 & -1 & 3 \end{vmatrix} = (+2u, 4u-3, -1) \xrightarrow[\text{other direction}]{\text{need}} \underline{n}(u,v) = (-2u, 3-4u, 1)$$

↳ step 3: calculate the scalar product

$$\begin{aligned} \vec{F}(r(u,v)) \cdot \underline{n}(u,v) &= (2u^2v + 4uv^2) + (6u + 3v - 8u^2 - 12uv) + (u^2 + 3v) \\ &= 6u + 12v - 7u^2 + 2u^2v + 4uv^2 - 12uv \end{aligned}$$

↳ step 4: use formula (1)

$$\text{is } \Rightarrow \int_0^3 \int_0^1 (-7u^2 + 2u^2v + 4uv^2 - 12uv + 6u + 12v) dv du$$

↳ step 4: use formula (1)

$$\iint_S \vec{F} \cdot d\vec{A} = \int_0^3 \int_0^1 (6u + 12v - 7u^2 + 2u^2v + 4uv^2 - 12uv) dv du$$

$$= 6 \cdot \frac{9}{2} + 12 \cdot \frac{3}{2} - 7 \frac{3^3}{3} + 2 \frac{3^3}{3} \cdot \frac{1}{2} + 4 \frac{3^2}{2} \cdot \frac{1}{3} - 12 \frac{3^2}{2} \cdot \frac{1}{2} = \underline{\underline{-30}}$$

Ex2 when you can use (2) If  $\vec{F}$  is constant &  $S$  is a plane figure

$A = (1, 0, 1)$   $S$  is the triangle determined by  $A, B, C$ ,  
 $B = (1, 1, 1)$  oriented "downwards"  $\vec{F}(x, y, z) = (5, 4, 3)$   
 $C = (2, 0, 3)$

According to (2) we need  $\text{area}(S)$  &  $\perp$  proj. of  $\vec{F}$  onto  $n$ .

we need two sides of the triangle

$$\begin{cases} \underline{b} := \vec{AB} = (0, 1, 0) \\ \underline{c} := \vec{AC} = (1, 0, 2) \end{cases}$$

$$\left. \begin{aligned} \text{then } \text{area}(S) &= \frac{1}{2} |\underline{b} \times \underline{c}|, \\ |\perp \text{proj}| &= \vec{F} \cdot \frac{\underline{b} \times \underline{c}}{|\underline{b} \times \underline{c}|} \end{aligned} \right\} \Rightarrow \frac{1}{2} \cdot \cancel{|\underline{b} \times \underline{c}|} \cdot \vec{F} \cdot \frac{\underline{b} \times \underline{c}}{\cancel{|\underline{b} \times \underline{c}|}}$$

$$= \frac{1}{2} \vec{F} \cdot (\underline{b} \times \underline{c})$$

check the orientation!

$$\underline{b} \times \underline{c} = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ 0 & 1 & 0 \\ 1 & 0 & 2 \end{vmatrix} = (2, 0, -1) \quad \checkmark \text{ OK since } 3^{\text{rd}} \text{ component} < 0.$$

triple product

$$\begin{vmatrix} F_1 & F_2 & F_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{vmatrix}$$

Thus flux =  $\frac{1}{2} \cdot \begin{vmatrix} 5 & 4 & 3 \\ 0 & 1 & 0 \\ 1 & 0 & 2 \end{vmatrix} = \frac{1}{2} \cdot (10 - 3) = \underline{\underline{\frac{7}{2}}}$

Reference: Thomas's Calculus Ch. 16.8&amp;

Gauss' divergence theoremGives an alternative way to calculate flux through a closed surface.Def! **divergence** of  $\vec{F} = (F_1(x, y, z), F_2(x, y, z), F_3(x, y, z))$  is the scalar function

$$\operatorname{div} \vec{F} = \frac{\partial}{\partial x} F_1 + \frac{\partial}{\partial y} F_2 + \frac{\partial}{\partial z} F_3 \quad (\text{notation } \operatorname{grad} \cdot \vec{F} = \nabla \cdot \vec{F})$$

Thm! **Gauss / divergence theorem**

Let  $\partial K$  be a piecewise smooth closed surface in space, which encloses the body  $K$ .  $\partial K$  is oriented outwards.  $\vec{F}$  is a vector field defined at every point of  $K$  (and whose components have continuous partial derivatives). Then

$$\iint_{\partial K} \vec{F} \cdot d\vec{A} = \iiint_K \operatorname{div} F \, dV.$$

Ex! physical interpretation of divergence

assume  $K$  is a ball around a point  $(x, y, z)$  with very tiny radius then we can say that  $\operatorname{div} F$  is approximately constant

The divergence then states  $\operatorname{div} \vec{F}(x, y, z) \approx \frac{\iint_{\partial K} \vec{F} \cdot d\vec{A}}{\operatorname{volume}(K)} = \frac{\text{flux "outwards"}}{\operatorname{volume}}$

If  $\operatorname{div} F(x, y, z) \begin{cases} > 0 & \Rightarrow (x, y, z) \text{ is a source} \\ < 0 & \Rightarrow (x, y, z) \text{ is a sink} \\ = 0 & \Rightarrow \text{same amount flows in and out} \end{cases}$

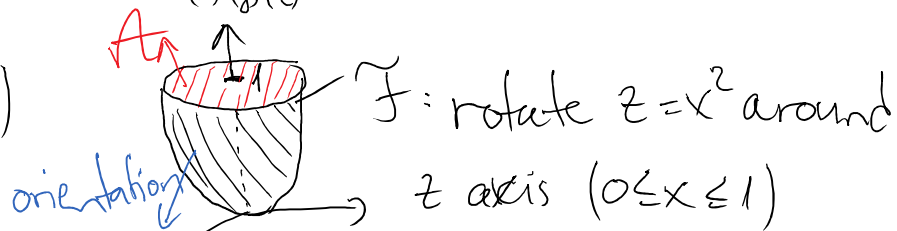
Another way to look at it:  $\vec{F}$  is the velocity field of flowing gas then  $\operatorname{div} \vec{F}$  gives the rate at which the gas is compressing ( $< 0$ ) or expanding ( $> 0$ ) at point  $(x, y, z)$ .

Ex2 Let  $K$  be the unit cube with surface  $\partial K$  pointing "outwards".  $\vec{F}(x,y,z) = (xy, yz, xz)$  Determine  $\iint_{\partial K} \vec{F} d\vec{A}$ !  
 We can use the divergence theorem ( $\vec{F}$  is nice) instead of having to calculate the flux for all 6 sides of  $\partial K$ .

$$\operatorname{div} \vec{F} = \frac{\partial}{\partial x} xy + \frac{\partial}{\partial y} yz + \frac{\partial}{\partial z} xz = x + y + z \quad \text{so}$$

$$\iint_{\partial K} \vec{F} d\vec{A} \stackrel{\text{Gauss}}{=} \iiint_K (x+y+z) dV = \int_0^1 \int_0^1 \int_0^1 (x+y+z) dz dy dx = 3 \int_0^1 x dx = \underline{\underline{\frac{3}{2}}}$$

Ex3.  $\vec{F} = (yz, xz, x^2 + y^2)$



Use the divergence

theorem to calculate  $\iint_F \vec{F} d\vec{A}$ !

$F$  is NOT a closed surface, but  $F \cup A$  IS! We can use the divergence theorem for  $\partial K = F \cup A$ , with  $A$  oriented "upward".

$$\iiint_K \operatorname{div} \vec{F} dV = \iint_F \vec{F} d\vec{A} + \iint_A \vec{F} d\vec{A}$$

$$\operatorname{div} \vec{F} = 0 \implies \iint_F \vec{F} d\vec{A} = - \iint_A \vec{F} d\vec{A} \quad \text{enough to calculate this!}$$

•  $A = \{(x,y,z) : x^2 + y^2 \leq 1, z=1\}$  parametric:  $x = r \cos \varphi$   
 $y = r \sin \varphi$   $z = z$   
 $0 \leq r \leq 1, 0 \leq \varphi \leq 2\pi$

$$\text{so } \underline{r}(r, \varphi) = (r \cos \varphi, r \sin \varphi, 1) \implies \vec{F}(\underline{r}(r, \varphi)) = (r \sin \varphi, r \cos \varphi, r^2)$$

$$\underline{r}'_r = (\cos \varphi, \sin \varphi, 0) \implies \underline{r}'_r \times \underline{r}'_\varphi = (0, 0, r)$$

$$\left. \begin{aligned} \underline{r}'_r &= (\cos\varphi, \sin\varphi, 0) \\ \underline{r}'_\varphi &= (-r\sin\varphi, r\cos\varphi, 0) \end{aligned} \right\} \Rightarrow \underline{r}'_r \times \underline{r}'_\varphi = (0, 0, r)$$

this is in the direction  
of the orientation

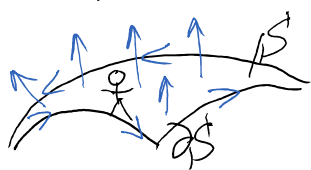
$$\Downarrow \iint_A \vec{F} d\vec{A} = \int_0^1 \int_0^{2\pi} \vec{F}(r, \varphi) \cdot \underline{n} \, d\varphi dr = \int_0^1 \int_0^{2\pi} r^2 \cdot r \, d\varphi dr = 2\pi \cdot \frac{1}{4} = \frac{\pi}{2}$$

$$\text{Thus } \iint_{\underline{F}} \vec{F} d\vec{A} = \underline{\underline{-\frac{\pi}{2}}}$$

## Stokes' theorem Reference: Thomas' Calculus Ch. 16.7

Relates the surface integral of  $\text{rot } \vec{F}$  to the line integral around the boundary of  $S$  in counterclockwise direction.

Def 2 A surface  $S$  and its boundary  $\partial S$  are **directed coherently**, if someone walks around  $\partial S$  so that he/she is standing

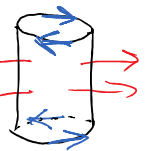


according to the orientation of  $S$ , then  $S$  is always on the left-hand side of the person.

Another way to say: if the thumb of a right-hand points in the direction of the orientation of  $S$ , then the fingers curl in the direction of  $\partial S$ .

Ex 4  $S =$  surface of a cylinder, orientation outwards

How to orient  $\partial S$  so that it is coherent with orientation of  $S$ ? on top clockwise  
on bottom counterclockwise



Thm 2 Stokes' theorem  $\vec{F}$  is a vector field.

Assume  $S$  and  $\partial S$  are directed coherently, furthermore, the partial derivatives of  $\vec{F}$  are defined in every point of  $S$ .

Then  $\boxed{\iint_S \text{curl}(\vec{F}) d\vec{A} = \int_{\partial S} \vec{F} d\vec{r}}$

Remark Most of the time  $\partial S$  consists of a single curve. But more than one is possible, see Ex4. Even  $\partial S = \text{empty set}$  is possible: think  $S = \text{surface of a sphere}$ . Then  $\int_{\partial S} \vec{F} d\vec{r} = 0$ , so  $\iint_S \text{curl}(\vec{F}) d\vec{A} = 0$  for any nice  $\vec{F}$ .

Ex5  $S = \{(x, y, z) : x^2 + y^2 \leq 1, z = 0\}$  unit disk on  $xy$ -plane oriented with normal vector pointing "upward"  
 $\partial S = \text{unit circle oriented counterclockwise}$

$$\vec{F} = \frac{1}{\sqrt{x^2 + y^2}} (y, -x, 3z) \quad \int_{\partial S} \vec{F}(c) d\vec{r} = ?$$

Can we use Stokes' theorem? NO, because  $\vec{F}$  is not defined at the origin.  $\text{rot}(\vec{F}) = (\text{something}, \text{something}, 0)$

$$\underline{n} = (0, 0, \text{something})$$

$$\Rightarrow \text{rot}(\vec{F}) \cdot \underline{n} = 0 \Rightarrow \iint_S \text{rot}(\vec{F}) d\vec{A} = 0$$

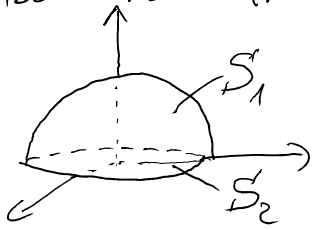
But  $\int_{\partial S} \vec{F}(c) d\vec{r}$  can be computed directly.  $\uparrow = -2\pi$   
 exercise for home

Ex6  $S_1 = \{(x, y, z) : x^2 + y^2 + z^2 = 9, z \geq 0\}$  hemisphere

$S_2 = \{(x, y, z) : x^2 + y^2 \leq 9, z = 0\}$  disk on  $xy$ -plane, radius = 3

Both have the same boundary  $\partial S = \{(x, y, z) : x^2 + y^2 = 9, z = 0\}$

Both have the same boundary  $\partial S = \{(x, y, z) : x^2 + y^2 = 9, z = 0\}$



$\vec{F} := (y, -x, 0)$  Assume  $S_1, S_2$ , and  $\partial S$  are oriented coherently.

Stokes  $\Rightarrow \iint_{S_1} \text{rot } \vec{F} \, d\vec{A} = \iint_{S_2} \text{rot } \vec{F} \, d\vec{A} = \oint_{\partial S} \vec{F} \, d\vec{r}$

Calculation of  $\oint_{\partial S} \vec{F} \, d\vec{r}$ :  $\partial S \quad \underline{r}(t) = (3 \cos t, 3 \sin t, 0)$

$\underline{\dot{r}}(t) = (-3 \sin t, 3 \cos t, 0)$

$$\oint_{\partial S} \vec{F} \, d\vec{r} = \int_0^{2\pi} 3 \sin t (-3 \sin t) + (-3 \cos t) 3 \cos t \, dt = \int_0^{2\pi} -9 \, dt = \underline{\underline{-18\pi}}$$

Remark physical interpretation of  $\text{rot}(\vec{F})$

Let  $P$  be a point in space,  $S_g$  a disk around  $P$  with a very tiny radius  $g$  and unit normal vector  $\underline{n}$ .

$\rightarrow$  can take  $\text{rot}(\vec{F}) \approx \text{rot}(\vec{F}(P))$  constant on  $S_g$

Stokes  $\Rightarrow$

$$\frac{\underline{n}}{|\underline{n}|} \cdot \text{rot}(\vec{F}(P)) \approx \frac{\oint_{S_g} \vec{F} \, d\vec{r}}{\text{area}(S_g)}$$

orthogonal proj. of  $\text{rot}(\vec{F}(P))$  onto  $\underline{n}$